

# Step up transformers

## Summary

The step up transformer is a simple and effective way to amplify the cartridge's signal adding very low noise and distortion; a close look to its details explains the mechanism behind a good and a bad match and the effect of the load on the secondary winding. Cartridge's and transformer's electrical characteristics play a key role and can generate an ultrasonic resonance or a response damped at high frequencies, an accurate tuning of the resistor at the output of the transformer can smooth this irregularity. Eventually, fine-tuning by ear will allow the listener to select the best match according to her/his personal preferences.

## The electrical model of the cartridge and step up

A moving coil cartridge can be modelled as voltage generator with an internal resistance  $R_{\text{cartridge}}$ , ranging from a few ohms to several tens, and an inductance  $L_{\text{cartridge}}$ , from few  $\mu\text{H}$  to  $100\mu\text{H}$  and more. Typically, lower output cartridges have smaller coils and hence lower resistance and inductance. The transformer is more complex and more parameters must be included in the model:

$L_p$  – inductance of the primary winding, 0.1H to 2H typically

$L_s$  – inductance of the secondary winding, the ratio of  $L_{\text{ess}}/L_p$  equals the square of transformer ratio

$R_{\text{pw}}$  – resistance of primary winding, a few ohms

$R_{\text{sw}}$  – resistance of secondary winding, several hundreds of ohms

$L_{\text{ss}}$  – stray inductance of the secondary winding, in the range of 10mH

$C_{\text{ss}}$  – stray capacitance of the secondary winding, a few hundreds pF

$C_{\text{pss}}$  – primary to secondary stray capacitance, a few hundreds pF

$N_p$  – number of turns of primary winding

$N_s$  – number of turns of secondary winding

For the sake of simplicity parasitic capacitance and leakage inductance of primary winding are omitted. Figure 1 shows the electrical model of the cartridge and a 1:10 step up transformer with typical values for the C, L and R parameters. The loading resistor  $R_{\text{load}}$  is assumed to be the standard 47k found in most preamplifier.

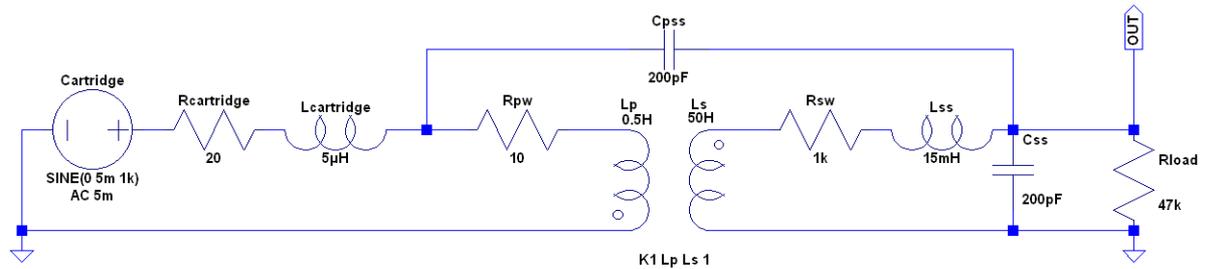


Fig. 1 Cartridge electrical model on the left, transformer model in the middle and loading resistor Rload on the right. 'K1 L<sub>p</sub> L<sub>s</sub> 1' is the spice command that simulates a perfect magnetic coupling of primary to secondary.

### The influence of cartridge parameters

As anticipated, the stray inductance and capacitance of the cartridge will generate a peak in the frequency response. In our model a +3dB resonance appears at 55kHz, well above the 20kHz limit but its effects can be starting from 10kHz and generate a +0.75dB deviation at 20kHz.

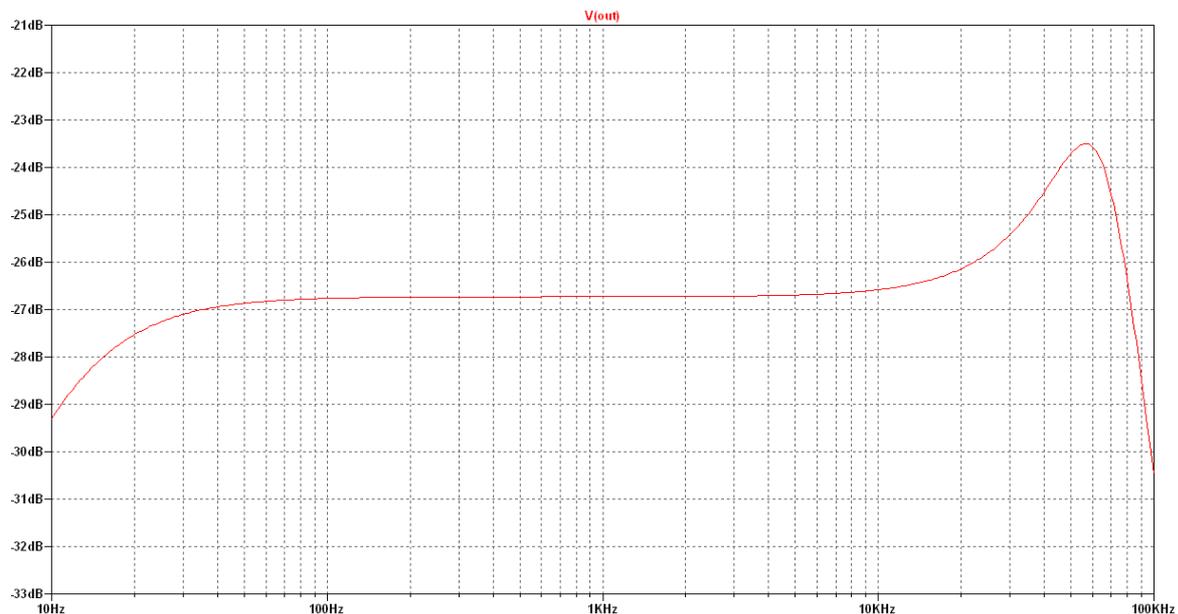


Fig. 2 A resonance of the cartridge-step up appears at 55kHz.

$R_{\text{cartridge}}$  and  $L_{\text{cartridge}}$  will have an influence upon the resonance: a large  $R_{\text{cartridge}}$  will exhibit a small resonance but high frequency response will be impaired for higher values; a larger inductance will move the peak towards the 20kHz limit affecting the audio band.

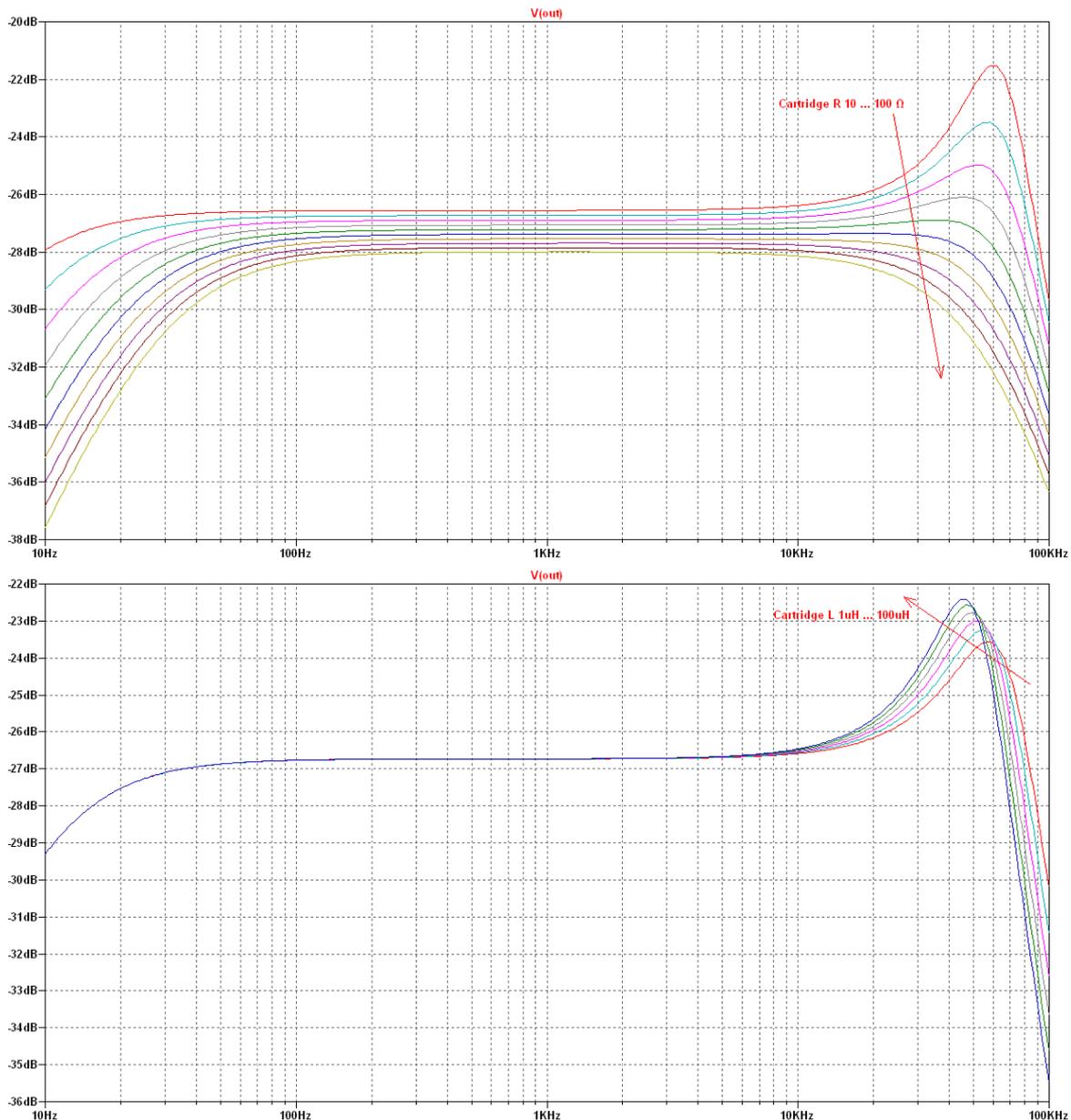


Fig. 3 and 4 Effect of cartridge parameters on the frequency response of the combined system. In figure 3, the low frequency response is impaired for higher  $R_{\text{cartridge}}$  that would require higher  $L_p$  for a proper match.

### Tuning the load at the secondary winding

$R_{\text{load}}$  will appear at the cartridge reduced by the square of the transformer ratio  $(N_p/N_s)^2$  so the 47k  $R_{\text{load}}$ , reflected by the 1:10 step up, looks like a 470Ω at the primary. A 20k will be stepped down to 200Ω and so on. A lower load will reduce the peak but a too small load will affect high frequencies as the transformer will not work in its best condition. The optimal load depends on the specific cartridge and step up. A flat frequency response might not correspond to the preferred sound and listener is encouraged to tune  $R_{\text{load}}$  according to her/his taste and sensibility.

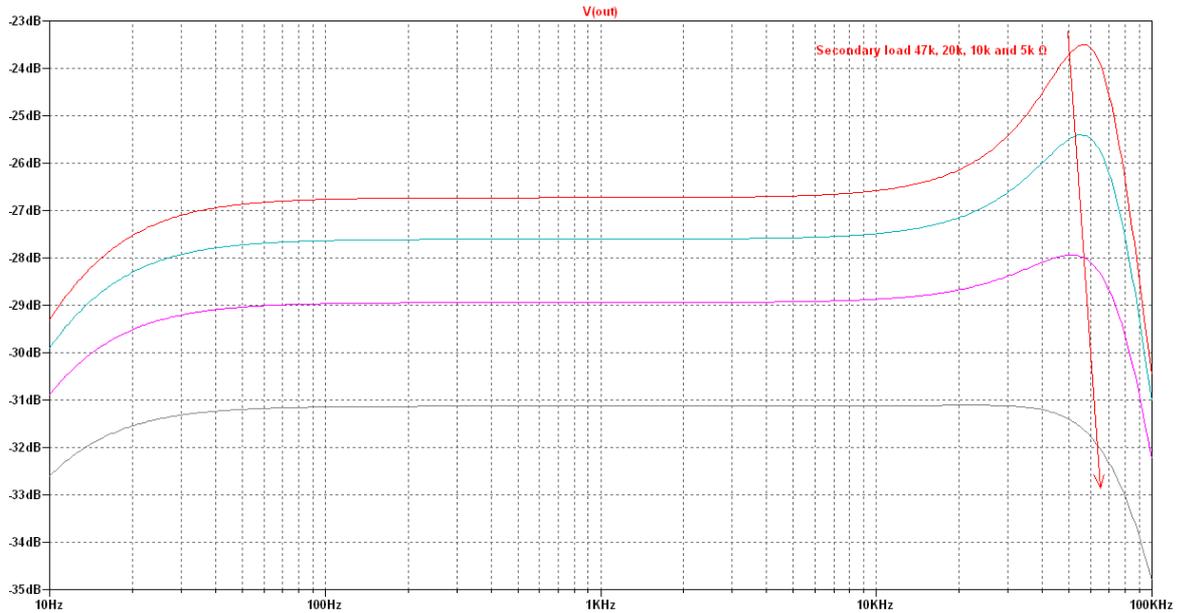
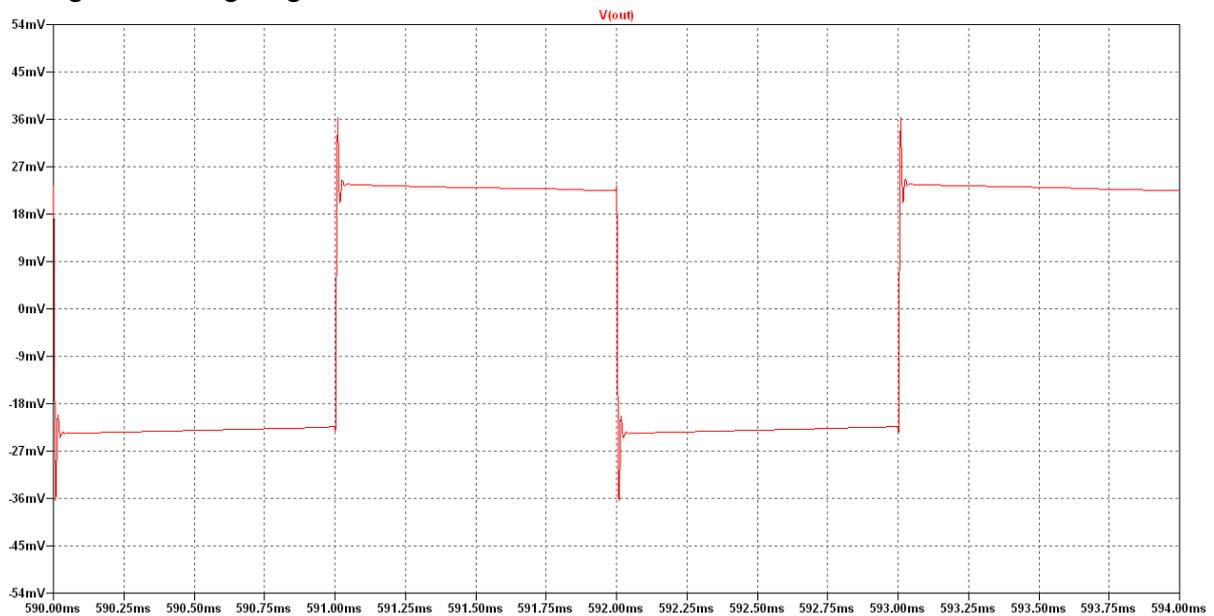


Fig. 5 Effect of reduced load on the cartridge-step up frequency response.

In figure 5, you will also notice as lower  $R_{load}$  will diminish the available signal due to the insertion loss, this can somehow confuse the listener as the phenomenon might be interpreted as a loss in dynamics. Figure 6 and 7 show the effects of  $R_{load}$  during a square test: the lower  $R$  dampens the resonance and the ripple at the rising and falling edges.



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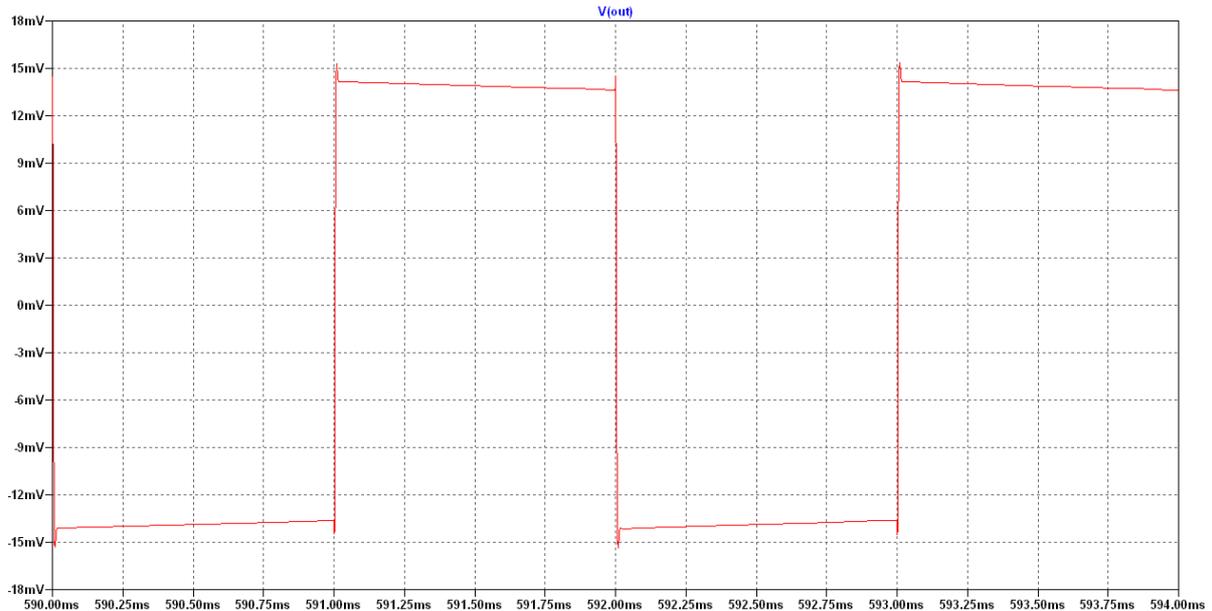


Fig. 6 and 7. 1kHz square wave response for a 47kΩ (upper fig) and 5kΩ (lower fig)  $R_{load}$ : the undamped resonance with 47kΩ generates a higher ripple.

### The best step up transformer

A good transformer must have reasonably low stray C and L and a sufficiently high primary inductance  $L_p$  for an extended flat bandwidth.

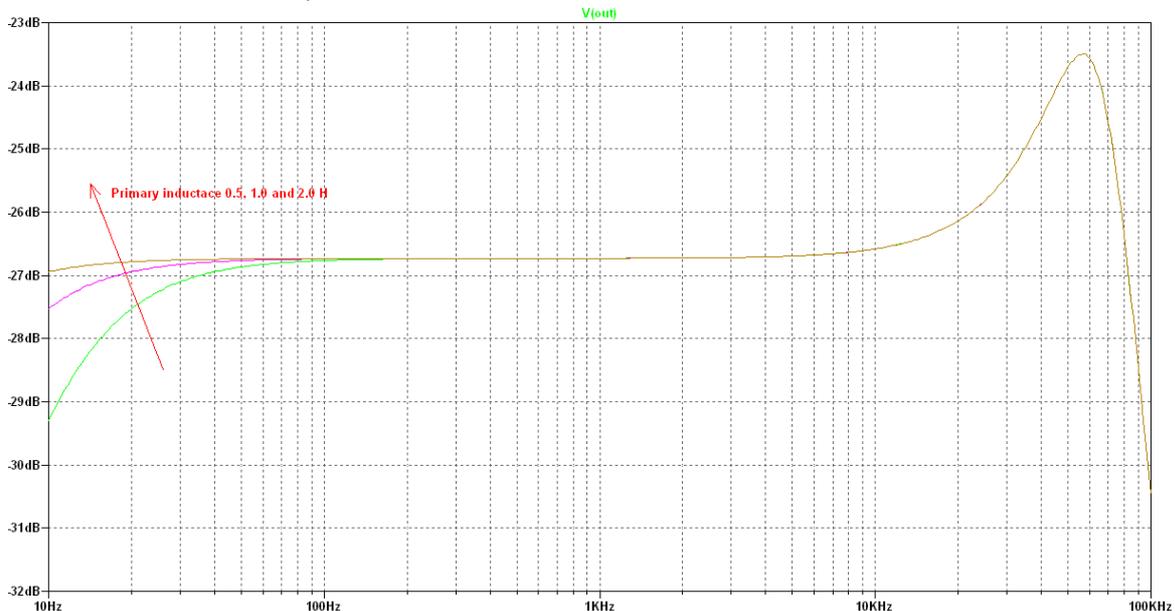
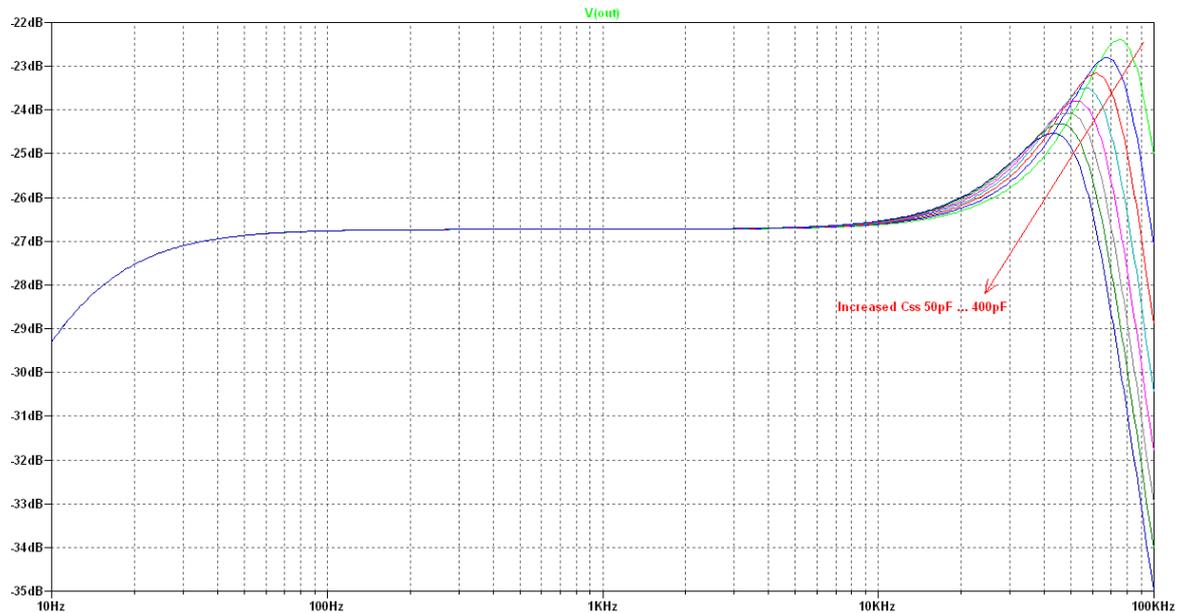
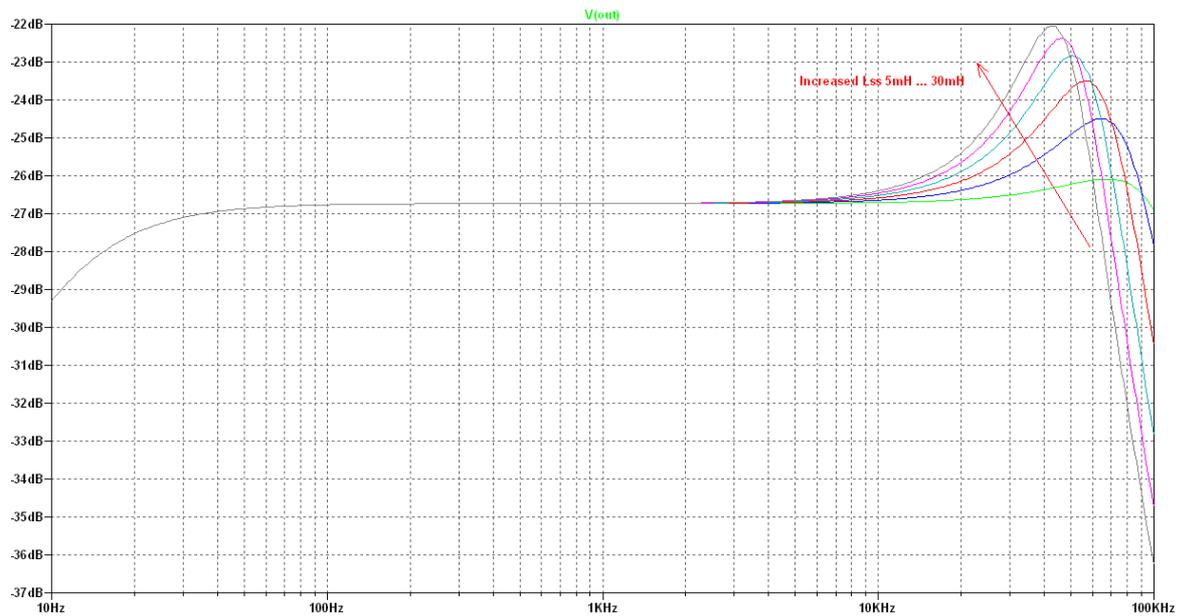


Fig. 8 Higher  $L_p$  extends into deeper bass the transformer's bandwidth.

A higher  $L_p$  is required to properly load high  $R$  cartridges, see also figure 3, and this should be the very first parameter to check when selecting a step-up. At low frequency  $f$  the transformer behaves as the parallel of the reflected  $R_{load}$  and of the primary reactance  $2\pi fL_p$ ; in this example at 20Hz we have 470Ω in parallel with 62Ω for an equivalent resistance of 55Ω substantially higher than the 20Ω cartridge.

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The effect of  $C_{SS}$ ,  $L_{SS}$  and  $C_{SSP}$  is similar: higher stray capacitance and inductance will move the resonance closer to the audio band affecting the response from 10kHz onwards and making the tuning of  $R_{load}$  even more critical. Leakage inductance is proportional to the  $N^2$  while special winding techniques are employed to reduce parasitic capacitance: a good transformer is the result of years of experience and experimentations.



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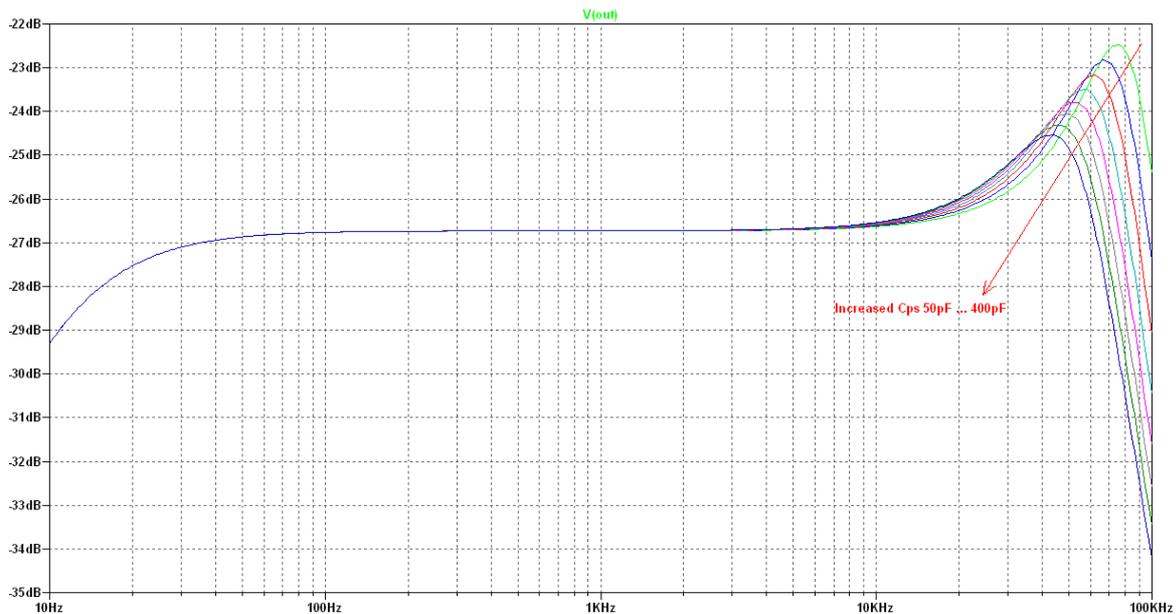


Fig. 9, 10 and 11 Effect of stray C and L on cartridge-step up frequency response.

### The core of the transformer matters

Primary inductance is proportional to the square of turns  $N_p$ , to the cross section of the core, to the magnetic path and to the permeability of the core material; the designer has to determine the best balance of core size and number of turns to assure the transformer will operate with low distortion and extended frequency range. Unfortunately, increasing the number of turns will also increase the flux density bringing the core closer to the saturation at low frequencies. On the other hand, a bigger core will have a larger cross section and a longer magnetic path but will also determine an increase of stray capacitance.

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